



Great Lakes Maritime Research Institute

*A University of Wisconsin - Superior and
University of Minnesota Duluth Consortium*



Update and Plans for Ballast-Free Ship Concept Development

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FY 2010 Goal: clarify economic and operational issues related to the
use of the Ballast Free Ship concept

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Ballast-Free Ship Design

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The Ballast-Free Ship Concept

- Traditional approach: Add water ballast to tanks to increase vessel weight in the light cargo condition
- Paradigm shift: instead of thinking add weight, reduce buoyancy
- **Ballast-Free Ship concept principles:**
 - Replace traditional ballast tanks with longitudinal, structural ballast trunks that extend beneath the cargo region below the ballast waterline.
 - Connect trunks to the sea through a plenum at the bow and another at the stern. Trunks flooded in ballast condition. Pumped when finished.
 - The natural hydrodynamic pressure differential between the bow and the stern region at speed induces a slow flow in the ballast trunks.
 - Trunks are, therefore, always filled with **“local seawater.”**
- US Patent #6694908, 2004

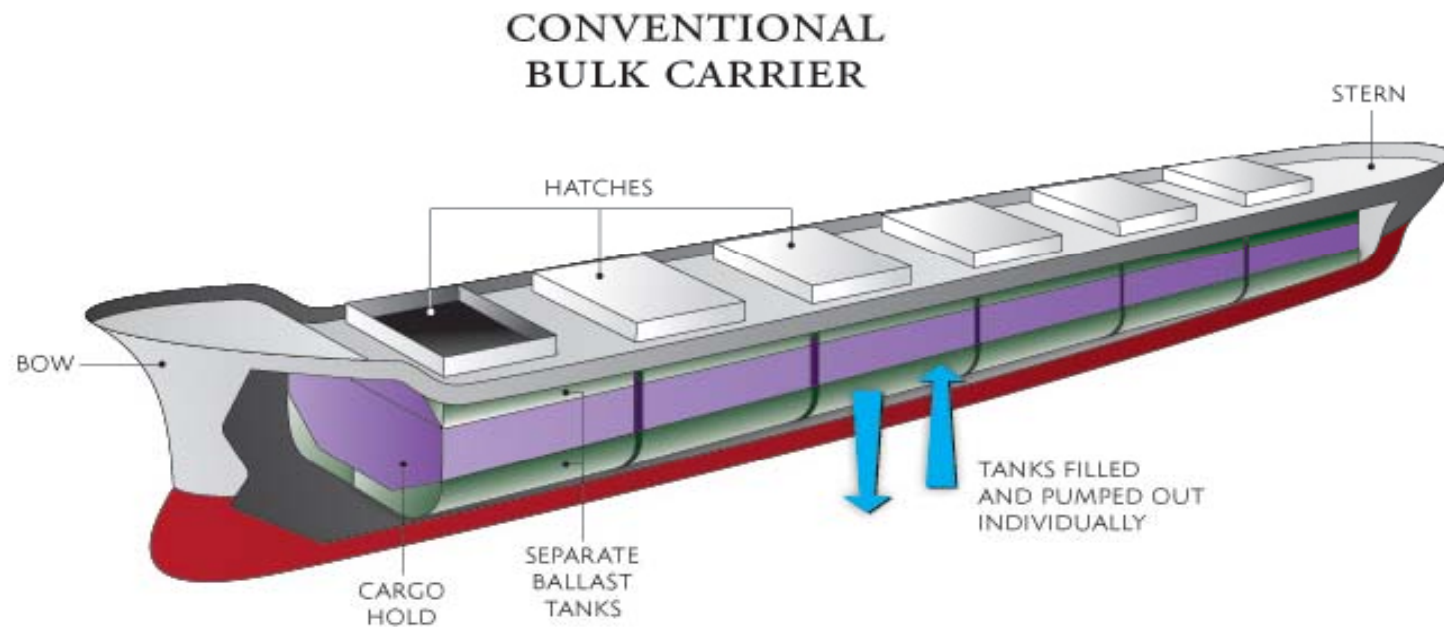
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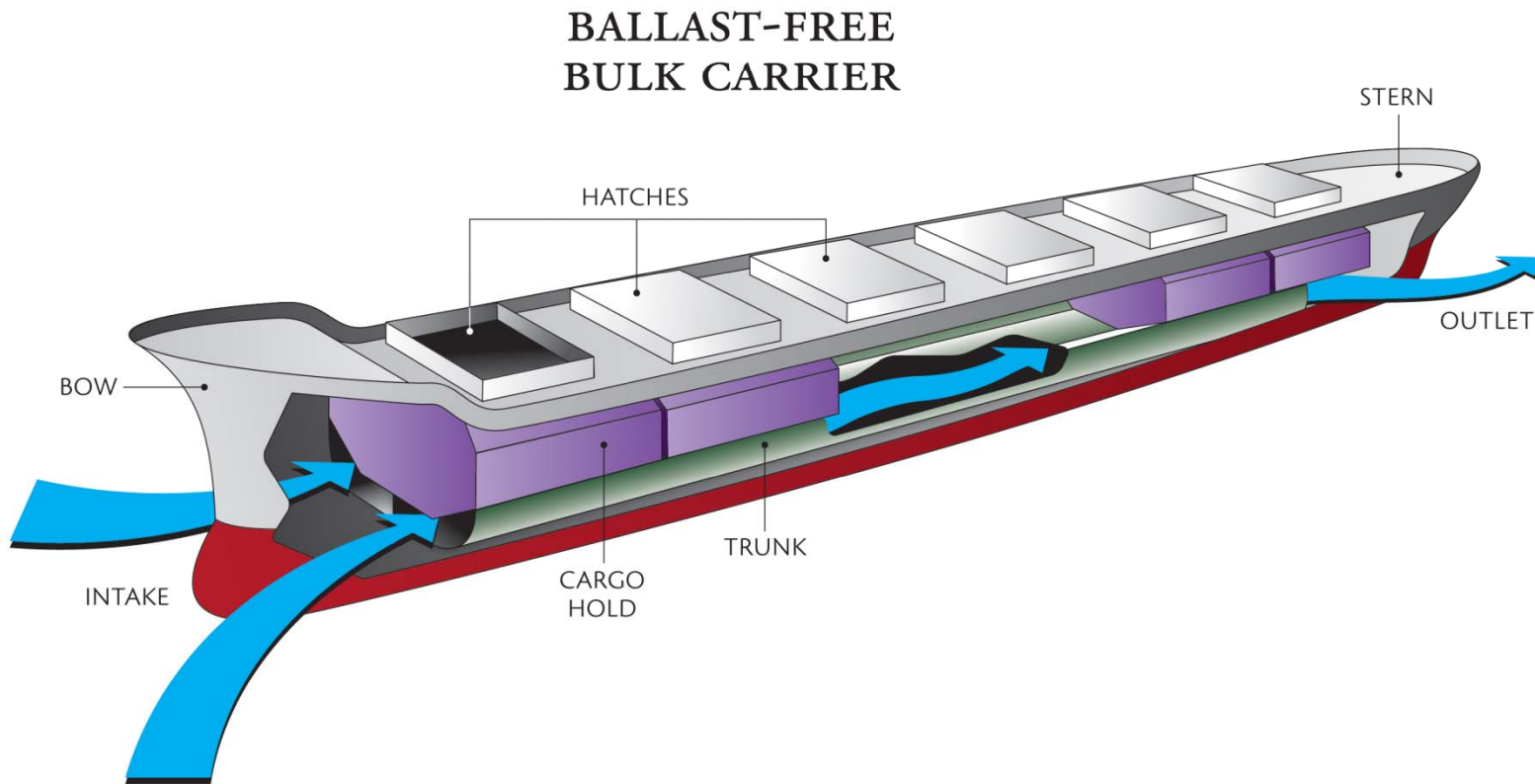
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Conventional Bulk Carrier Ballast



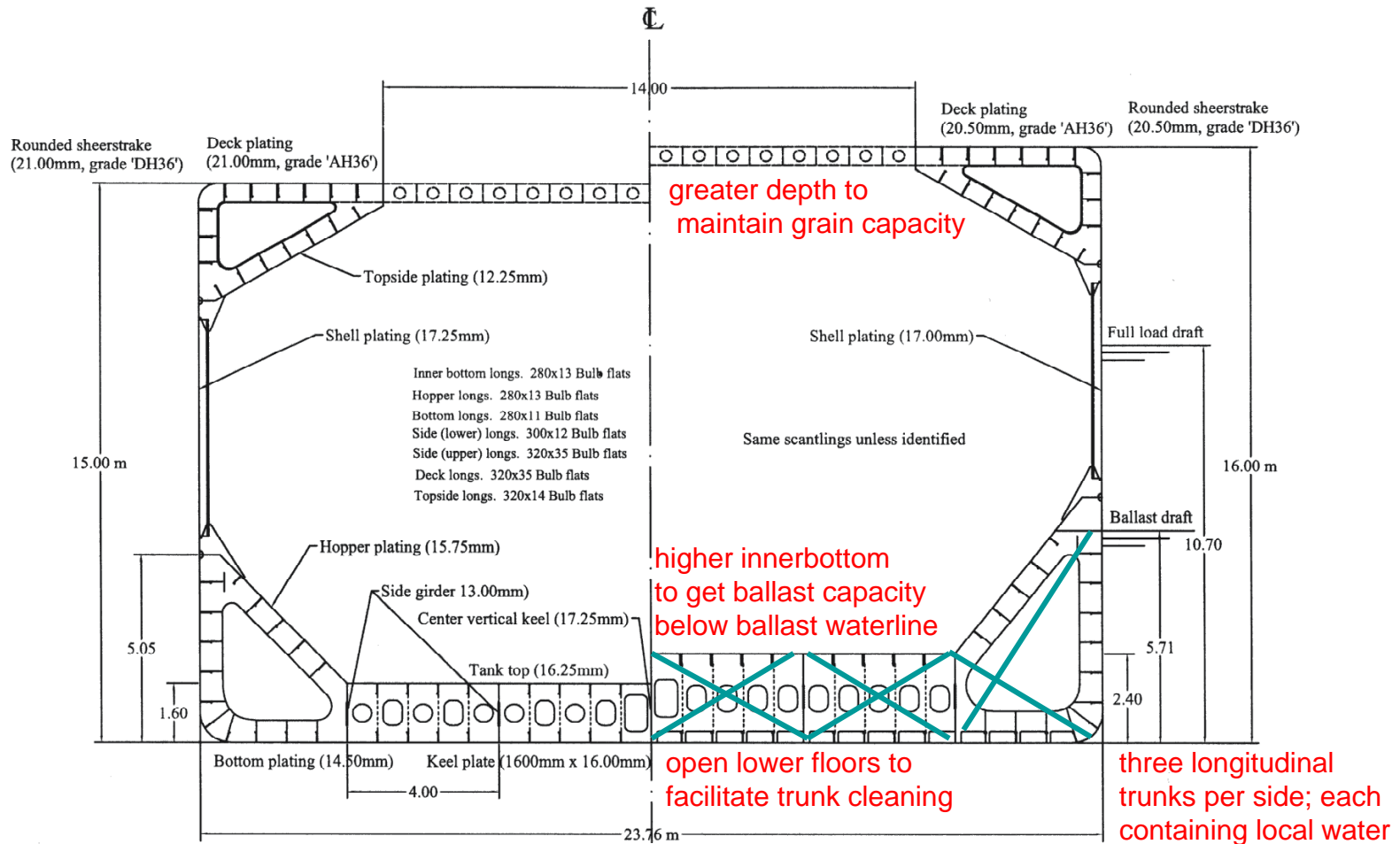
Ballast Free Bulk Carrier



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Comparison of Midship Sections



Typical Single-hull Salty Bulkcarrier

Ballast-Free Ship Design



Goals of the Past GLMRI Effort

- Design Ballast-Free ship Seaway-sized bulk carrier
- Build a precision scale model for use in subsequent hydrodynamic tests (FY2006),
- Optimize the location and details of the plena openings, particularly aft, in order to,
- Reduce the large propulsion power penalty (+7.4%) found in earlier National Sea Grant study (FY2007)
- Confirm and better explain the suspiciously large power decrease (-7.3%) observed in FY2007 (FY 2008)

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Seaway-sized Bulk Carrier Hull Form Design

- Design based upon:
Polsteam *Isa*
design from Jiangnan



LWL = 195.5 m
LBP = 192.0 m
B = 23.76 m
D = 16.0 m
 T_{FL} = 10.7 m

Block C_B = 0.835
Waterplane C_{WP} = 0.909
Displacement = 42,546 t

Ballasted to 40% fwd; 70% aft
Speed in ballast = 15.5 knots

Scale Ratio $\lambda = 37.92$ (5 m model)

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Five Meter (16.9' LWL) Scale Model



FY2006 Result



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Intake and Discharge Locations – July '08



Tip of bulb for maximum
input pressure

FY2007 and FY2008 Testing



STA17 – forward engine room bkhd

STA19 – aft engine room bulkhead



Increased Resistance with Trunk Flow



FY2008 Result



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Required Power Comparison

- Effective Power (resistance)/ η_D = Delivered Power

up 4.51%

?

what really matters \$\$

- Propulsive efficiency $\eta_D = \eta_O \eta_R \eta_H = \eta_P \eta_H$

- Open water propeller efficiency η_O

- Relative rotative efficiency η_R

- Hull efficiency $\eta_H = (1 - t)/(1 - w)$

- Baseline $\eta_D = \overset{\eta_O}{0.487} \times \overset{\eta_R}{1.0126} \times \overset{\eta_H}{1.0876} = 0.536$

- STA 17 $\eta_D = 0.522 \times 0.9593 \times 1.1380 = 0.570$

up

down

up

+6.27%

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Order of Magnitude Economic Comparison

	Typical bulk carrier	Ballast-Free bulk carrier
Installed engine Nominal MCR (kW)	8,580	
Block coefficient	0.835	0.841
Required service MCR in ballast (kW)	7,700	7,575
Hull steel weight (tonnes)	5,553	5,767
CRF (i = 10%, 20 yrs.)	0.1175	
Case: Roundtrip Rotterdam; Seaway draft; discharge at Station 17 compared with filtration and UV treatment <u>when ballast exchange is no longer allowed</u>		
Net capital cost change (\$)	- 476,400	lowered
Net operating cost change per annum (\$)	-116,920	fuel savings
Change in RFR (\$/tonne)	- 1.03	

almost \$1 per tonne grain (1%) cheaper to operate

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RFR = Required Freight Rate needed to make a profit
 annual cargo capacity 168,000 t grain



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Conclusions from Testing in FY2008

- Jan. 2007 STA17 improvement of -7.3% was incorrect
- Detailed analysis of changes in components showed inconsistent behavior compared to STA19 test and July 2008 test
- There is an increase in resistance (+4.5%) at STA17
- There can be a decrease in required power (-1.6%)
- Ballast-Free Ship concept can result in a significant savings compared to filtration and UV treatment etc. when ballast exchange is no longer allowed
- Still an issue of the effects of using stock propellers

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Publications from GLMRI Effort

Short Invited Articles

Maritime Reporter

Great Lakes/Seaway Review

2008 Yearbook of Maritime Technology (Scandinavia)

Papers

Kotinis, M. and Parsons, M. G., "Hydrodynamic Investigation of the Ballast-Free Ship Concept" SNAME Annual Meeting, Ft. Lauderdale, Nov. 2007; in *Transactions SNAME*, **115**, 2007.

SNAME ABS/Captain Joseph H. Linnard Prize for the Best 2007 Paper

Kotinis, M. and Parsons, M. G., "Hydrodynamics of the Ballast-Free Ship Revisited," Great Lakes and Great Rivers Section Meeting of SNAME, Ann Arbor, MI, Nov. 13, 2008; submitted to *Marine Technology*

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Goals for Coming Year FY2010

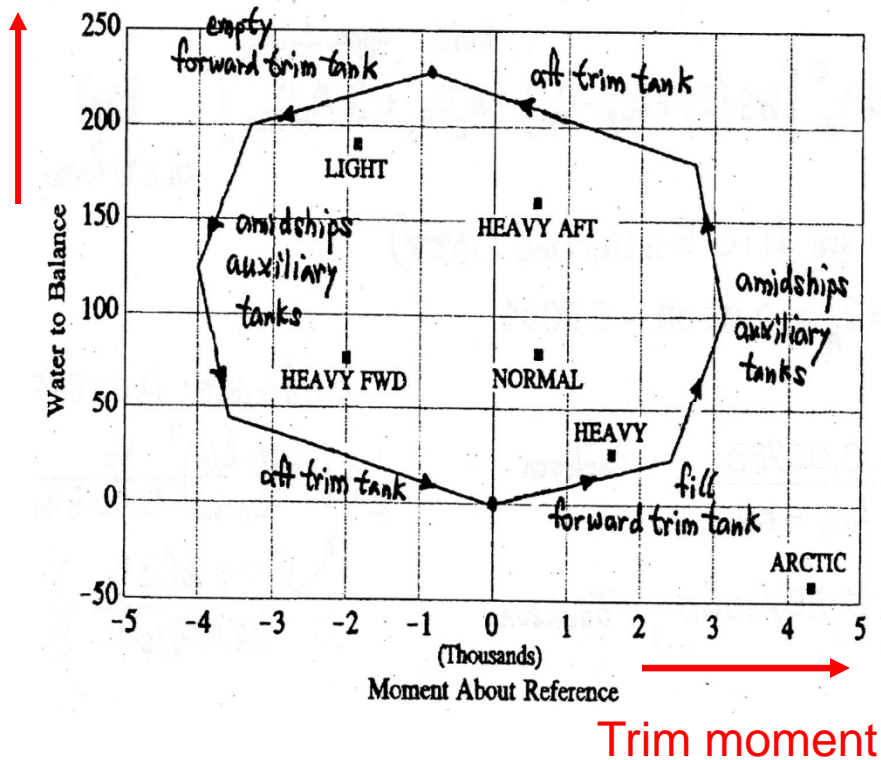
- Propulsion Investigation using Custom Propeller Design
resolve issue of stock versus optimum propeller
further clarify expected power/fuel savings (- \$\$)
Computational Fluid Dynamics (CFD) analyses
propeller design, rapid prototyping, MHL testing
- Details and Flow Resistance of Trunk Isolation Valves
early work used sluice valves – industry criticism
new design with motor operated butterfly valves
- Operations Capabilities of Trim/Draft Control
control is discrete (trunk segments full or empty)
versus continuous (various levels in ballast tanks)

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Capability to be Displayed with an Adaptation of Submarine Equilibrium Diagrams

Weight or draft change



- Draft change versus trim moment envelope

Cases:

- Discrete segments from ends only (full or empty)
- Added piping (\$\$) to allow any discrete segment
- Use piping to fill segments to any level

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Thank You

Questions?

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